

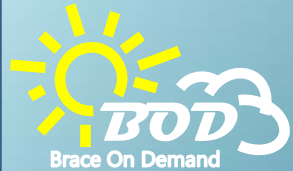
Brace On Demand

A Cloud Service for Seismic Design of
Buckling Restrained Braces and Connections

Assistant Researcher, NCREE
Ming-Chieh Chuang



Using WES-BRBs for An Improved Seismic Resisting Performance of Buildings
Auckland/ Wellington/Christchurch, New Zealand. Nov. 12~14, 2013



BOD Cloud Service



HTTP
Port:80, 8080

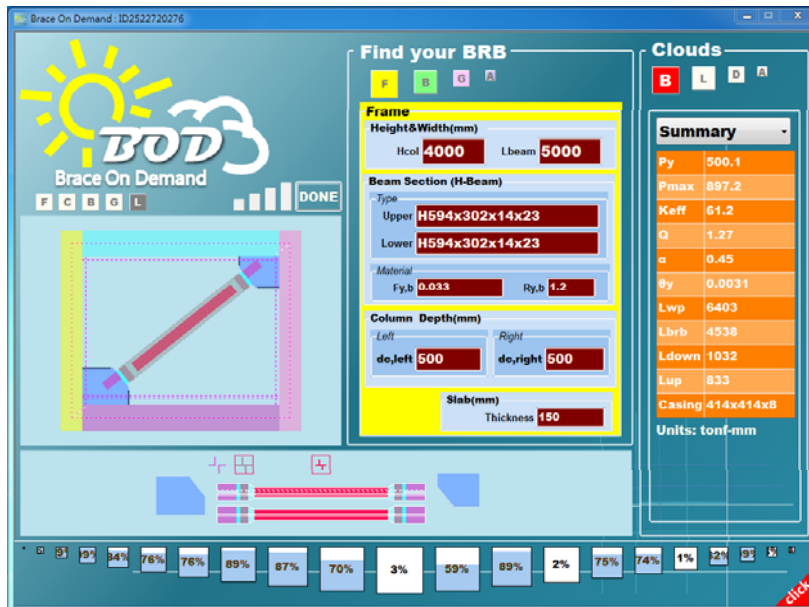
Server

On-demand service

Space, Strength and Stiffness

Diagonal & Chevron Config. BRBFs

<0.1sec. (in Taiwan)



Client

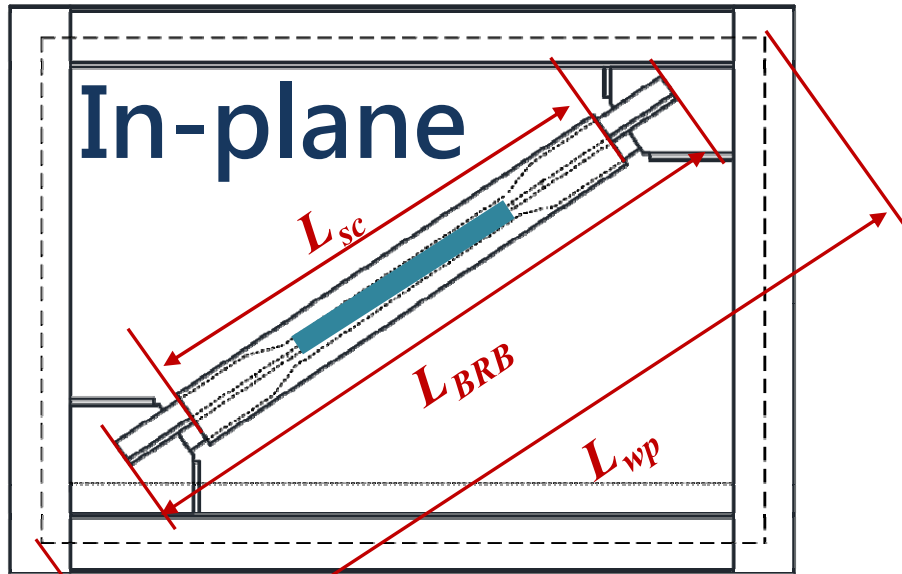
bod.ncree.org.tw

No set up required!

Friendly user interface

Portal to download structural calculations

Space Demand (Frame geometry)



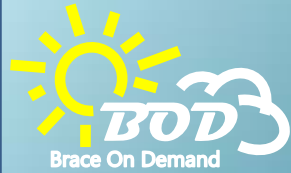
$$I_{sc} \geq \frac{P_{max} L_{sc}^2}{\pi^2 E}$$

In-plane:

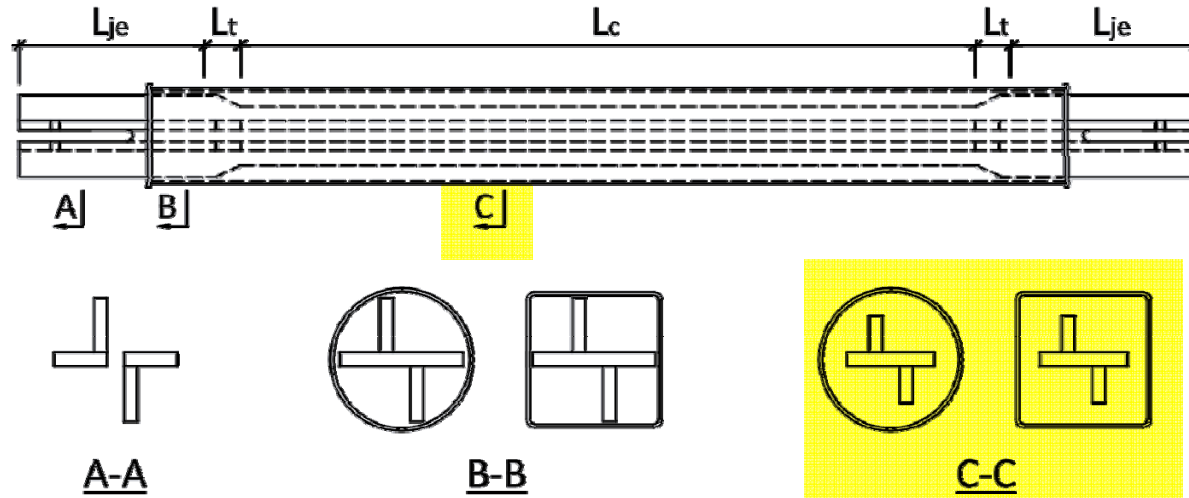
The longest L_{BRB} , L_c and L_{sc}
 The best fatigue life (max. α_c)
 The minimum K_{eff}

Out-of-plane: The casing size (Width)





Strength Demand ($P_y=75\sim1500\text{tonf}$)



4 characters to customize your **WES-BRB**.

Steel
Material

A36

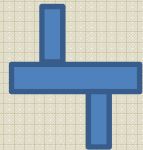
A572 GR50

SN490B/CM

X

Core
Type

Cruciform



Flat

X

Yield
Strength

(25 P_y levels)

Min/Max

100/**1500**

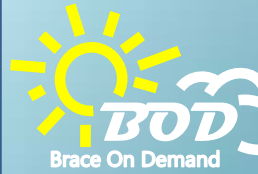
75/250

tonf

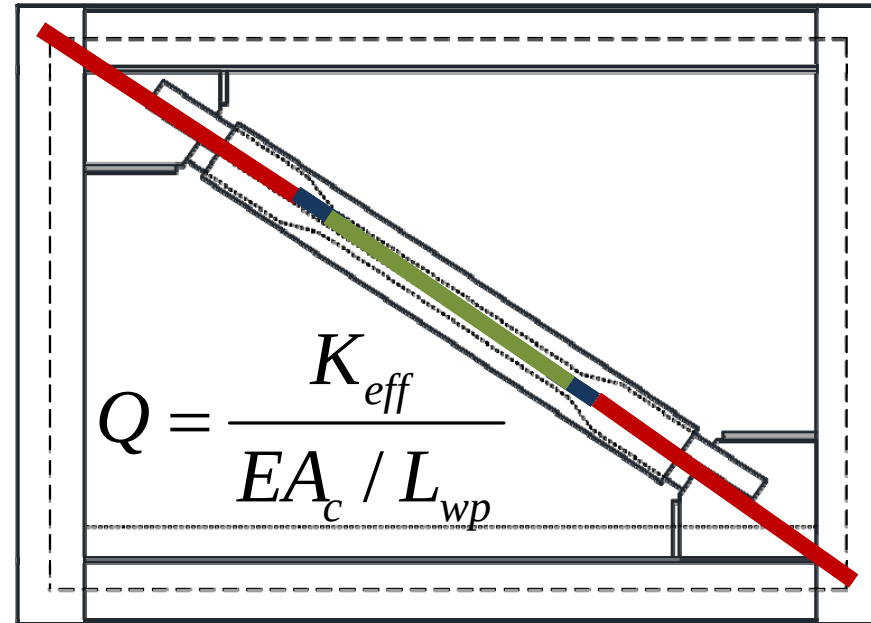
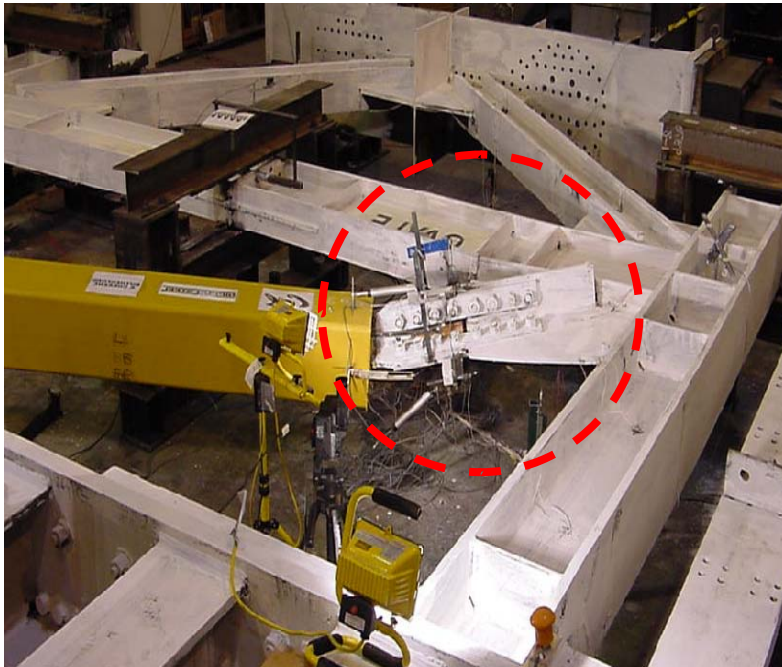
X

Type of
Casing



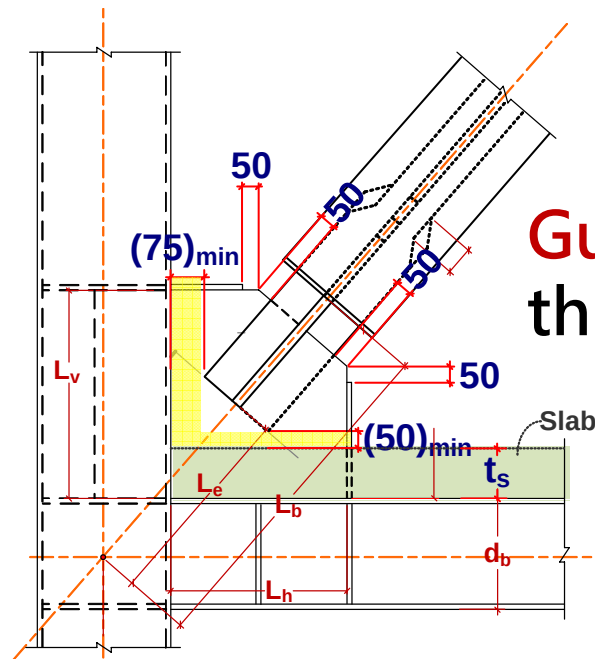
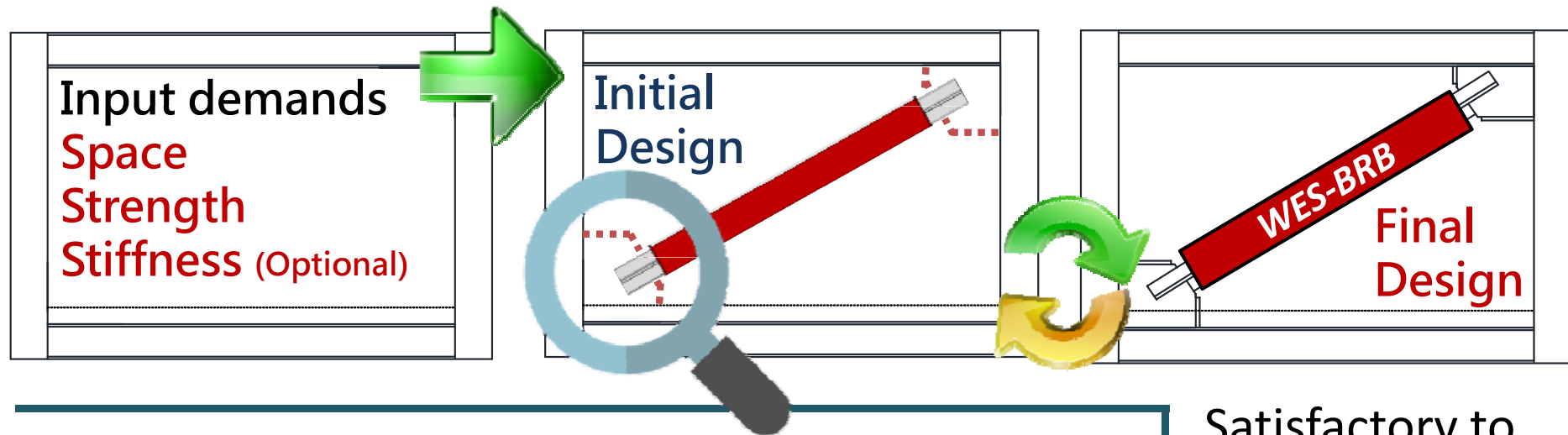


Stiffness Demand (User-specified K_{eff})



- *By default setting, BOD can find **the minimum K_{eff}** .
- *In general, **Q value** is ranging from **1.2~1.5**.
- *BOD allows you to **increase the K_{eff}** when **$Q < 1.6$ & $\alpha_c > 0.3$** .

Automated Design Procedure

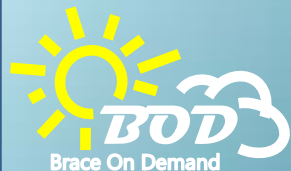


Gusset Plate thickness t_g = Core Plate thickness t_c

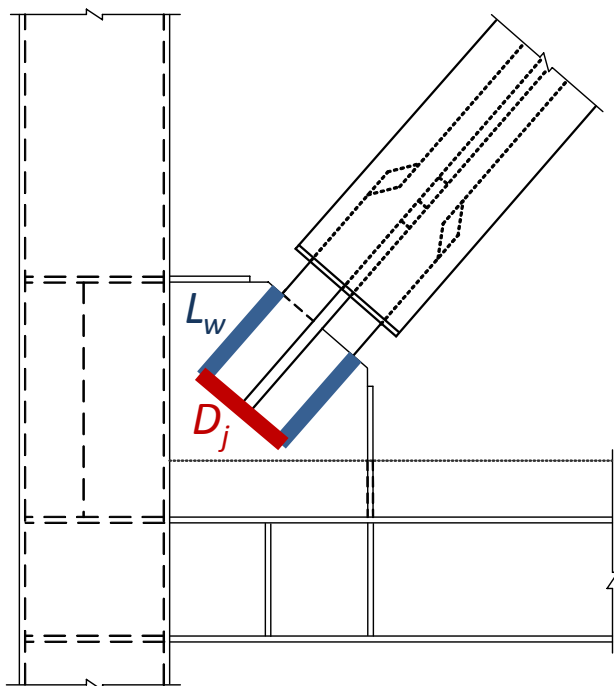
Satisfactory to

1 **21**
limit states

2 **K_{eff}**
User-specified



Strategies for Improving Design

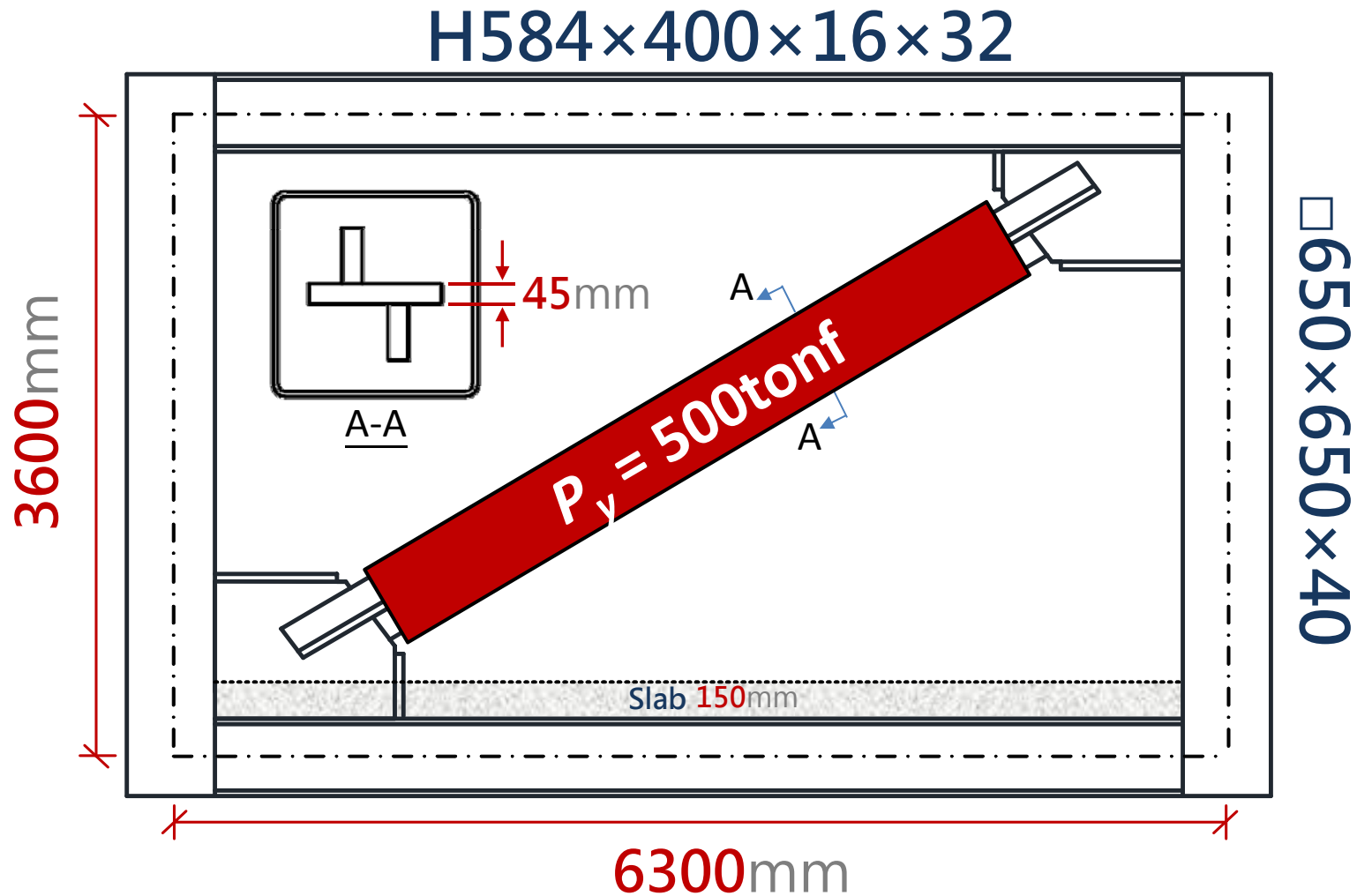


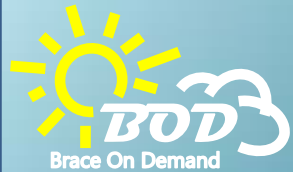
**Notable
Tradeoffs**



	Enlarge the Joint Region Size (D_j)	Increase the Welded Connection Length (L_w)	Increase the Gusset Thickness (t_g)
1. Steel Casing Buckling			
2. Joint Region Yielding	⊙		
3. Joint Region Buckling	⊙		
4. Gusset Plate Block Shear		⊙	⊙
5. Gusset Plate Yielding		⊙	⊙
6. Gusset Plate Buckling			⊙
7. Gusset to Beam/ Column interface Strengths			⊙
Effects on K_{eff}	+	+	-

The Example Case (SN490CM)





The Example Case (SN490CM)

Brace On Demand : ID2481131374

Find your BRB

Frame

Height&Width(mm)

Hcol **3600** Lbeam **6300**

Beam Section (H-Beam)

Type

Upper **H584x400x16x32**

Lower **H584x400x16x32**

Material

Fy,beam **0.033** Ry,beam **1.2**

Clouds

BRB

Type

Cruciform

Casing

Square Tube

Core Material

CNS SN490B/CM

Yield Capacity(tonf)

500tonf(tc=45mm)

Configuration

Diagonal

Yield Capacity(tonf)

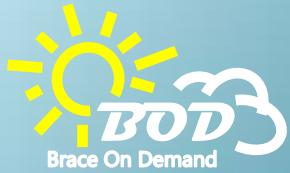
500tonf(tc=45mm)

Configuration

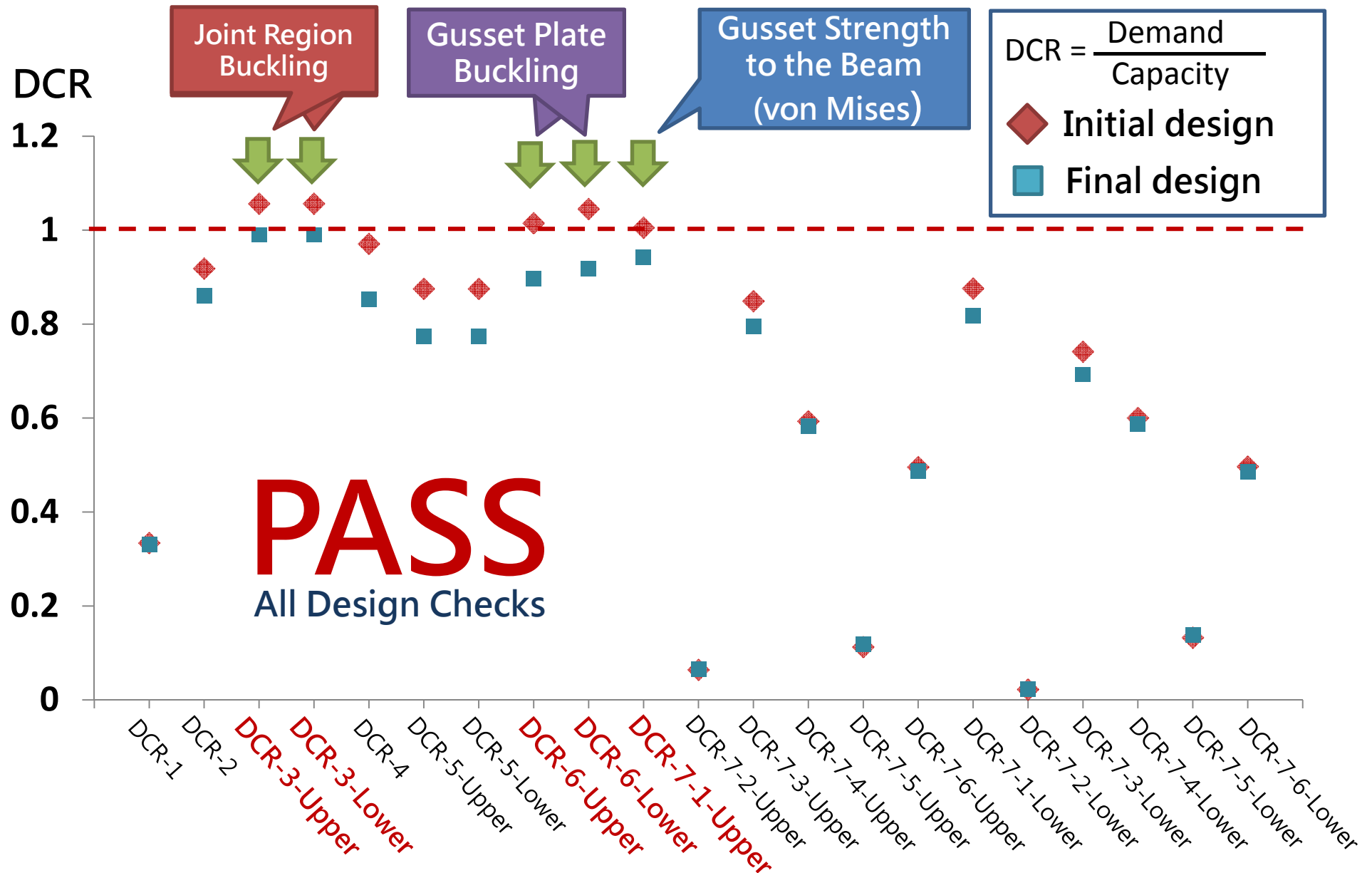
Diagonal

2% 9% 35% 77% 77% 89%

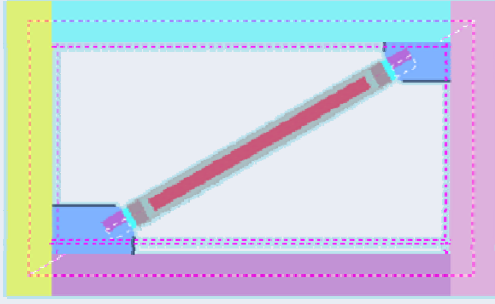
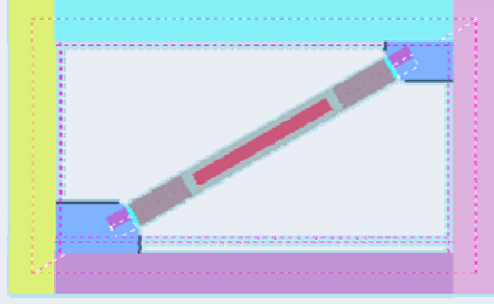
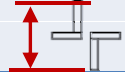
click

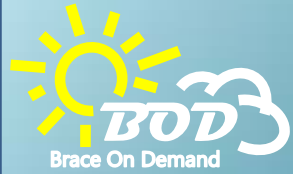


Results of Final Design (OK)



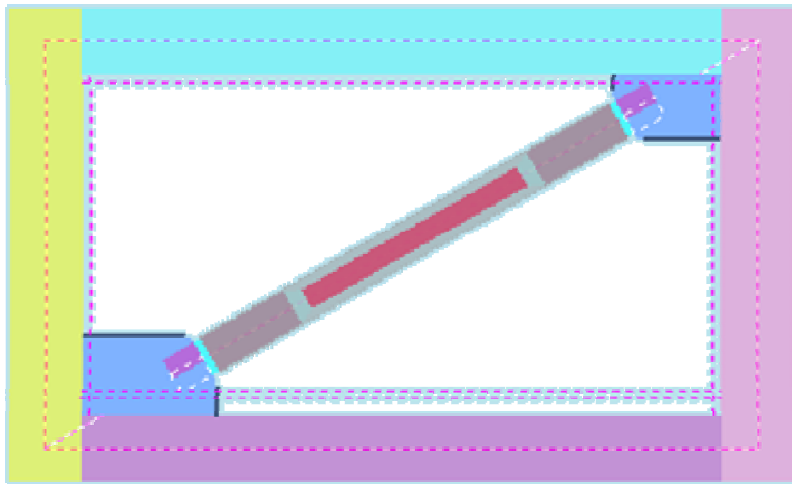
Results of User-specified K_{eff}

SN490CM	Default Final Design	User-specified K_{eff}
H_{col} : 3,600mm L_{beam} : 6,300mm Beams : H584×400×16×32 Columns : ☐ 650×650×40 BRB : $P_y = 500\text{tonf}$; $t_c = 45\text{mm}$		
L_{BRB} (mm)	4989	4939 ↓ -1%
L_c (mm)	3535	2193 ↓ -38%
α_c (L_c/L_{wp})	0.49	0.30 ↓ -38%
D_j 	305	333 ↑ 9%
Q	1.33	1.60 ↑ 20%
K_{eff} (tonf/mm)	57	68 ↑ 20%
Steel casing size (mm)	350×350×9	370×370×8 ↑ 6%
Gusset plate thickness (t_g)	50	50
Upper gusset plate weight (kgf)	185	196 ↑ 6%
Lower gusset plate weight (kgf)	288	302 ↑ 5%



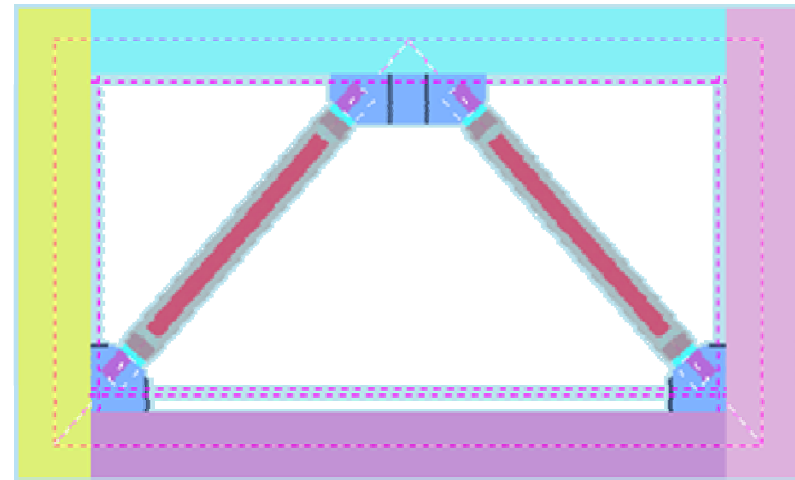
BOD Design Capabilities

Not only



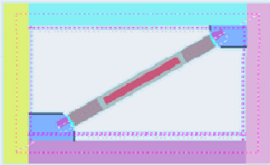
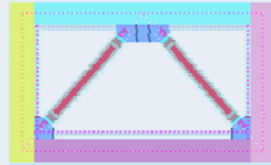
21
limit states

But also



33
limit states

Alternative of Chevron Configuration

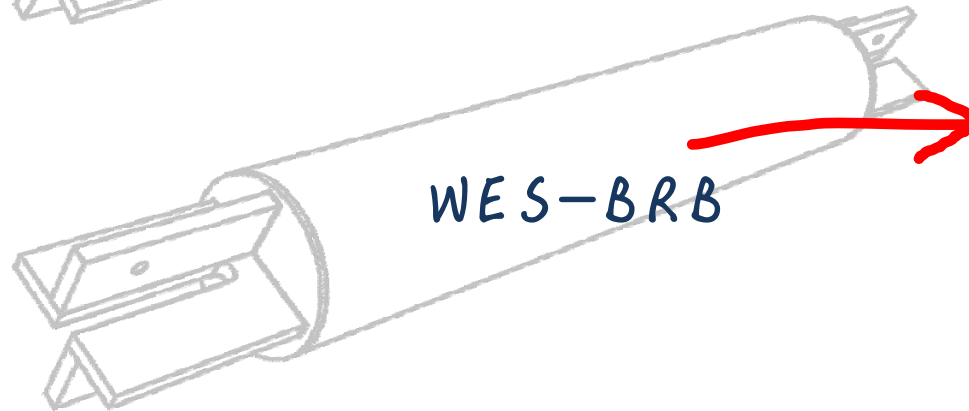
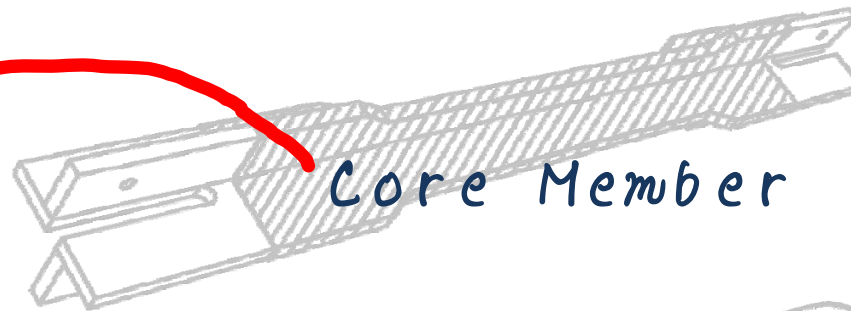
SN490B/CM	User-specified K_{eff}	Chevron Configuration
Φ (degree)	 29.7	 48.8
P_y (tonf)	500 ($t_c = 45\text{mm}$)	350 ($t_c = 40\text{mm}$)
L_{BRB} (mm)	4939	2744
L_c (mm)	2193	1690
α_c	0.30	0.37  23%
Q	1.60	1.44  -10%
K_{eff} (tonf/mm)	68	61
Steel casing (mm)	370×370×8	300×300×4.5  -19%
θ_y (% radian)	0.28	0.29
t_g (mm)	50	50
Horizontal stiffness $K_h = K_{eff} \cos^2 \varphi$ (tonf/mm)	51.3	52.5
Horizontal strength $V_y = P_y \cos \varphi$ (tonf)	434	461

WES-BRB Details

Core

Core	
Lc	3535
tc	45
Bc	191
Dc	191
Ac	15165
Transition	
Lt	115
At	20303
Joint	
Lj	612
Lx	192
Ln	96
Lw	324
Tw	36
tj	45
Bj	305
Dj	305
Aj	25441
End Slot	
Ls	349
tg,s	53

Units: tonf-mm



Casing

Type	350x350x9
Product	Available
Dt,req	343.2
Dt	350
t	9
Isc,req	7.68E+07
Isc	2.32E+08
Lsc	4149

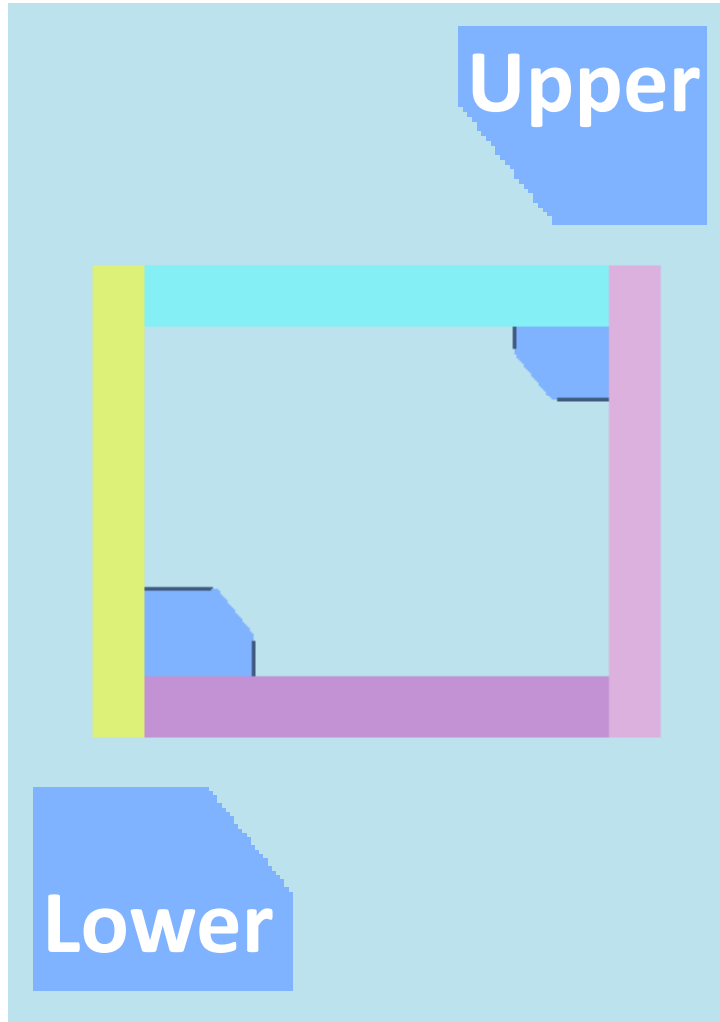
Units: tonf-mm

Summary

Py	500.4
Pmax	897.8
Keff	56.9
Q	1.33
α	0.49
θ_y	0.0034
Lwp	7256
L_BRB	4989
Le,lower	1259
Le,upper	1008
Casing	350x350x9

Units: tonf-mm

Details of Gussets



Gusset

Lower

tg	40
Lh	1062.3
Tb	29
Lv	832.5
Tc	23

Upper

tsf	20
Lsf,h	658.3
Lsf,v	340

Lower

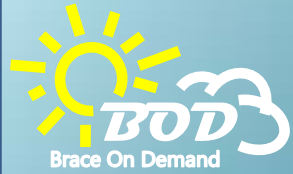
tg	40
Lh	906.3
Tb	32
Lv	707.7
Tc	25

Upper

tsf	20
Lsf,h	502.1
Lsf,v	215

Units: tonf-mm





Archives & Standard Drawings



txt

Structural
Calculations



xls

Spreadsheet



dwg

Standard
Drawing



pdf

Standard
Drawing

```

[Limit State 6]Gusset Plate Buckling(隅板挫屈破壊檢核)

[>>Inputted]
[Lower]
L1 = 556.6mm
L2 = 17.6mm
L3 = 366.9mm
(L1 + L2 + L3)/3 = 313.7mm
Lr = max( (L1 + L2 + L3)/3, 0) = 313.7mm
Be = 862.4mm
tg = 40mm
K factor = 0.65
λc = 0.23
Fcr,g = 0.9321tonf/mm²

One click to obtain

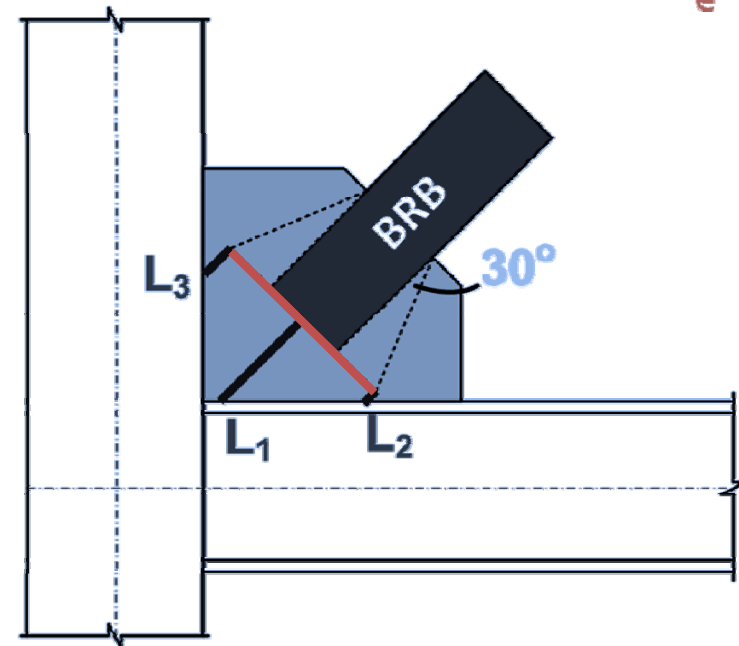
[<<Determined]
[Demand-6/Lower] = Pmax = 897.2tonf
[Capacity-6/Lower] = 0.9*Fcr,g*Be*tg = 1002.8tonf
[DCR-6/Lower] = 0.895
  
```

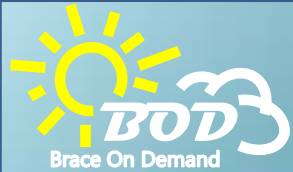
Gusset Plate Buckling

$$L_r = \frac{L_1 + L_2 + L_3}{3} \quad \lambda_c = \frac{KL_r}{\pi r} \sqrt{\frac{F_{y,g}}{E}}$$

$$\begin{cases} \lambda_c \leq 1.5, & F_{cr,g} = 0.658^{\lambda_c^2} F_{y,g} \\ \lambda_c > 1.5, & F_{cr,g} = \frac{0.877}{\lambda_c^2} F_{y,g} \end{cases}$$

Width of Whitmore section = B_e





Insights through EXCEL

Make the complete spreadsheet. **To a BOD.**

BOD-Diagonal-E

入 版面配置 公式 資料 校閱 檢視 Load Test PDF Team

標楷體 28 A⁺ A⁻ 自動換列

字型

Double check the accuracy

斜撐型式 Type of BRB	標稱降伏 Py(tonf)	極限壓力強度 Pmax(tonf)	等效勁度 Keff(tonf/mm)	勁度因子Q	耗能長度因子α	Hcol(mm)	Lbeam(mm)
Welded End-Slot BRB	500.4	897.8	56.86	1.33	0.49	3600.0	6300.0

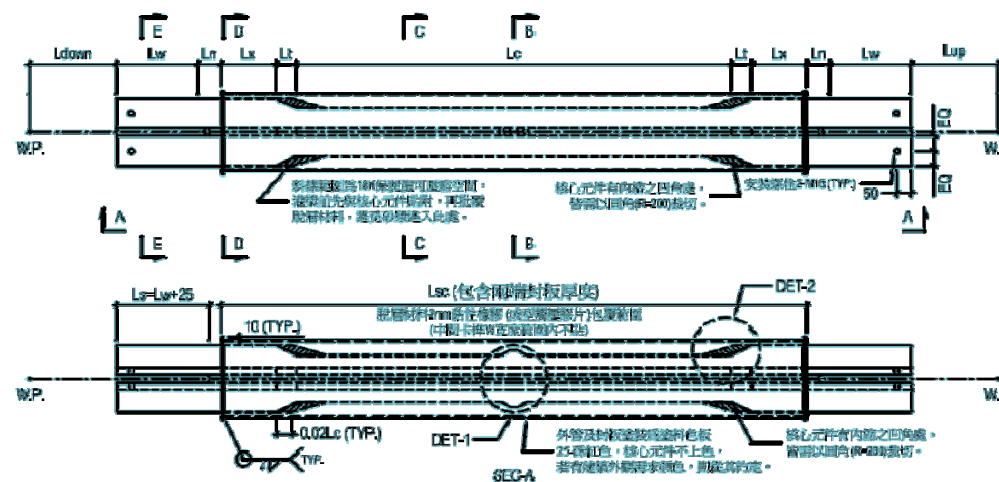
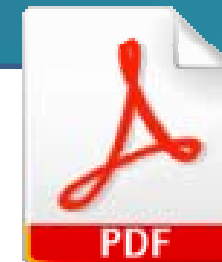
Server: S13101901 Template: ver2013-16 Date: 2013/10/18

<<DEFAULT SETTINGS>>

tonf-mm	tonf/mm^2
20.4	
0.049	

<<SUMMARY>>

Yielding strength: Py	=P16*B52
Thrusting compressive axial force capacity: Pmax	=J11*B53*B54*B55
Effective stiffness: Keff	
Effective stiffness factor: Q = Keff/(EAo/L)	=B12*P16*P19*P29/
Energy dissipation section length ratio:	



<http://BOD.ncree.org.tw>

SEC-B

SEC-C

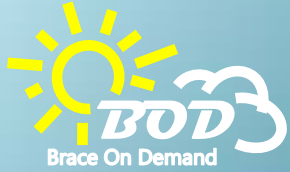
SEC-D

SEC-E

DET-1

DET-3

內灌8000psi之無收縮水泥砂漿或自充填混凝土
(自充填混凝土之骨材粒徑以12-13mm為宜，且不得大於19mm)

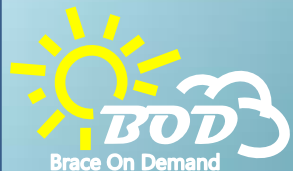


Conclusions

BOD could **reduce the iteration work**, and **enhance the engineers' productivity**.

The innovative archives using **EXCEL** make the computing **"transparent"** .

By using **cloud computing**, any **up-to-date** service can be achieved.



Thank you



<http://BOD.ncree.org.tw>

